

# **Rigging Design Guide**



1.866.899.4090

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-

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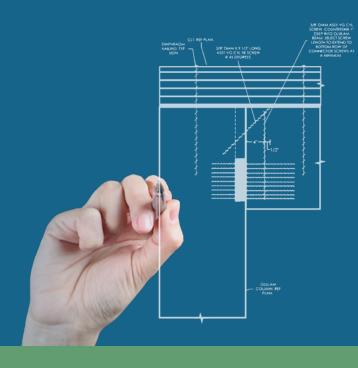
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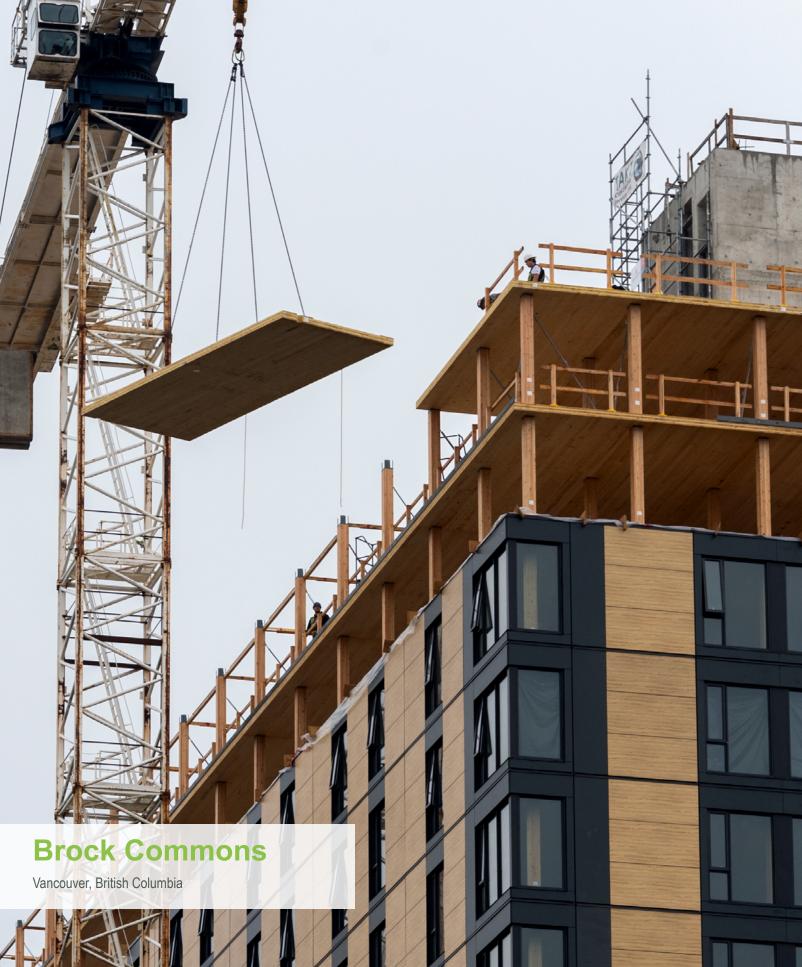
Use our comprehensive & practical resources to find the most cost-effective solutions for your structural elements.





# TESTED & PROVEN SOLUTIONS

Count on MTC Solutions' 10+ years of expertise, providing tested & proven ICC approved solutions, support, and resources.



# **General Information**

## The MTC Solutions Rigging Systems

The MTC Solutions Rigging Systems are one-of-a-kind rigging solutions designed to lift timber elements of various weights, dimensions, and materials. These lab-tested solutions utilize high-quality code-approved ASSY self-tapping screw fasteners to provide reliable lifting capacities. The anchor configurations and fast installation of the self-tapping screws allow these systems to be some of the most efficient mass timber rigging systems on the market.



## Lab-Tested Solutions

The MTC Solutions Rigging Systems are lab-tested solutions for mass timber rigging, meeting the ISHA safety standards for hoisting and rigging products. Additionally, the screw fasteners used with MTC Solutions Rigging Systems hold an ICC-ES and CCMC approval. All systems have undergone testing up to the ultimate failure using North American timber materials and have been used in many prominent mass timber projects across North America.



# **Rigging System - Selection Tool**

The following pre-selection table is intended to give the reader an overview of different rigging scenarios and MTC Solutions Rigging Systems by listing allowable lifting capacities for common lifting applications. The appropriate sections should be consulted for more information on specific rigging scenarios. When lifting construction elements, other lifting requirements such as anchor end and edge distances and potential rigging hazards must be considered.

Table 1, Yoke Rigging Anchor Selection Tool

e					
Transp	oort Anchor	Mini Yoke	Yoke 1T	Yoke 5T	Yoke XL
Option A: Light Frame Panel Riggi	ng				
Structural Insulated PanelPrefabricated I-Joist FloorPrefabricated Stud Wall					
Option B: Mass Timber Floor / Roc	f Panel Riggin	g			
CLT Panel up to 2,500 lbs[1]CLT Panel up to 12,900 lbs[1]CLT Panel up to 18,500 lbs[1]MPP Panel up to 16,000 lbs[1]					
Option C: Mass Timber Wall Panel	Tilting				
CLT Panel up to 6,500 lbs <sup>[2]</sup> MPP Panel up to 7,200 lbs <sup>[2]</sup>					<ul> <li>✓</li> <li>✓</li> </ul>
Option D: Glulam Beam & Log Rig	ging				
Glulam Beam Rigging	$\checkmark$				

Log Rigging

Notes: 1. Unfactored weight for CLT floor or roof panel rigging with 4 anchors and standard rigging scenario

2. Unfactored weight for CLT wall panel rigging with 2 anchors and standard rigging scenario

# How to Use This Guide

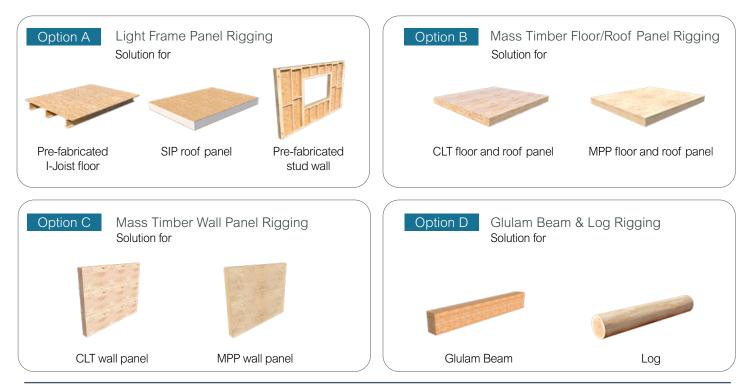
## Preparing a Rigging Plan

#### Step 1: Factoring Total Load

Determine the total factored load ( $W_r$ ) based on the weight of the panel and rigging conditions.

#### Step 2: Rigging System Selection

Determine the type of rigging needed;



#### Step 3: Safety Checks



#### Step 4: Installation Instructions



Notes:

1. The basic procedures proposed above contain the steps recommended for the licenced design professional to prepare a rigging plan.



All rigging elements shall be approved by a licensed design professional. All rigging shall be done by qualified personnel only. It is the responsibility of the rigger to ensure a safe work environment and verify the condition of all equipment. All suggestions and details shown in this guide are to be treated as general and cannot be assumed to be valid for all construction requirements and specific site conditions.

#### **Rigging Capacity**

- 1. Listed basic factored resistance values (N',) are only valid with their accompanying ASSY screws.
- Listed basic factored resistance values (N',) shall be factored with appropriate reduction factors as described on page 30.
- Listed basic factored resistance values (N', consider the capacity of the screws and rigging device.
- 4. Total rigging capacity of the anchoring devices  $(N_r)$  must be greater than the summation of all sling forces  $(S_T)$ .
- 5. The terms "anchor" and "anchoring device" refer to the rigging device and screws as a system.
- 6. To ensure full connection capacity in flat panel lifting, fasteners must penetrate panel plies to the largest extent possible, with a minimum of three plies penetrated.
- 7. In all rigging applications, the minimum penetration and wood panel thickness must be respected.

#### **Anchor Placement**

- 1. All anchor end and edge distance requirements are minimum requirements and must be respected during installation.
- 2. To ensure stable rigging with appropriate load sharing, the center of gravity shall be determined, and locations of the anchors shall be chosen accordingly.
- 3. Additional moment equilibrium calculations are required to determine the proportion of the total factored load shared by each anchor for situations where anchors are not spaced equidistant around the center of gravity.



#### **Rigging Slings and Load Spreader**

- 1. The resultant forces in each sling must be calculated separately and must not exceed the basic factored resistance values (N',) of the anchoring devices.
- 2. Slings must lift elements at a minimum angle of 60° measured between the sling and the panel surface ( $\beta$ ). Otherwise, the capacity of the anchors shall be adjusted with the appropriate anchor resistance reduction factor  $(R_{AR})$  given in Table 22.
- 3. The anchor resistance reduction factor  $(R_{AB})$ accounts for the reduced capacity of the Yoke anchors at sling angles lower than 60° measured between the sling and the panel surface.
- 4. A load spreader/compensation system should be used for lifts using more than two anchors. Otherwise, the capacity of the anchors shall be adjusted with the appropriate load spreader reduction factor  $(R_{I,s})$  or other appropriate engineering judgment.

#### **Rigging Condition Requirements**

- To ensure safety and proper capacity, the fasteners 1. used for panel rigging must only be used once.
- 2. Proper inspection should be performed frequently on the anchoring devices to ensure their structural integrity. If damages are found on the anchors, the device must not be used and must be taken out of circulation immediately.
- 3. Before each lift, check proper sling attachment
- 4. The load line should be transferred over to the element's center of gravity before the lift.
- 5. No object or person should be present on the element during rigging (no live load).
- 6. Suspended loads must be securely attached and properly balanced before they are set in motion
- 7. The load must always be kept under control. The use of taglines is recommended to prevent uncontrolled motion.
- 8. Loads must land safely and properly blocked before the element is unhooked and unslung
- 9. No overhead lifting at anytime.
- 10. Maximum installation torque of rigging screws is shown in Table 2.

5.	It is the responsibility of the rigging professional								
	to ensure	the	working	limits	of	the	slings	are	
	respected								

Table 2, Fastener Torsional Strength

Screw Diameter [ D ]	1/4" 5/16"		3/8"	1/2"
	[ 6 mm ]	[ 8 mm ]	[ 10 mm ]	[ 12 mm ]
	5.9 ft∙lbf	13.6 ft·lbf	26.6 ft·lbf	38.5 ft·lbf
Maximum Torque	[7.3 N·m]	[ 16.7 N·m ]	[32.7 N·m]	[47.3 N·m]

# Step 1: Factoring Total Load

Determining the total factored load ( $W_f$ ) of the rigged element is essential. Actual loads must be factored up. The proposed method incorporates a dead load factor (1.4), a dynamic acceleration factor, and an optional safety factor to consider in each rigging scenario. In all cases, the total factored load ( $W_f$ ) shall be specified and approved by a licensed design professional.

$$W_{f} = 1.4 \cdot W \cdot K_{os} \cdot K_{v} \qquad (eq.1)$$

W

K<sub>os</sub>

Unfactored weight of the rigged element [kN or lbs]

• Provided in shop drawings or manufacturer's specifications

Optional safety factor :

•	For rig mat rigging	1
---	---------------------	---

- For open space rigging 1.2
- For tight space rigging 1.3

**K**<sub>ν</sub> Dynamic acceleration factor :

Table 3 provides recommended dynamic acceleration factors ( $K_v$ ) subject to approval by the licensed design professional.

Table 3, Proposed Dynamic Acceleration Factor, K

Crane Type	Dynamic Acceleration Factor [K,]
Fixed crane	1.1 to 1.3
Mobile crane	1.3 to 1.4
Bridge crane	1.2 to 1.6
Rigging and moving on flat terrain	2 to 2.5
Rigging and moving on rough terrain	3 to 4

Sources:

1. Pfeifer, Snaam, Halfen, Peikko, Arteon

In cases where information on weight is not provided, a calculation based on the dimensions and the wood species may be done to estimate the unfactored weight in pounds:

$$W = (h \cdot b \cdot I) \cdot G \cdot C' \qquad (eq.2)$$

h Element thickness [mm]

- **b** Element width [m]
- I Element length [m]
- **G** Assigned relative densities :

•	For SPF	0.42
•	For D-Fir	0.49

**C'** Unit conversion factor <sup>[1]</sup>:

For pounds (Ibs)	2.54
For kilonewtons (kN)	11.3 · 10 <sup>-3</sup>

Notes:

[1] The unit conversion factor contains adjustments from oven dry to standard dry service condition moisture content.

# **Brock Commons**

1

Vancouver, British Columbia

# Step 2: Rigging System Selection

Step 2, Option A: Light Frame Panel Rigging

### Structural Insulated Roof Panels Using Yoke Systems

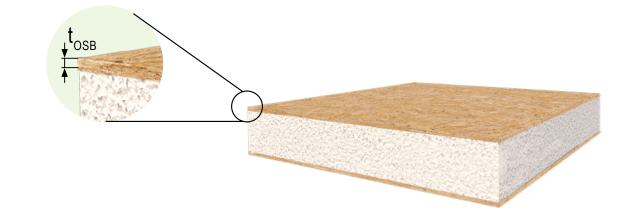
Table 4, Basic Factored Resistance Values for SIP Flat Panel Rigging Using Mini Yoke (N',)

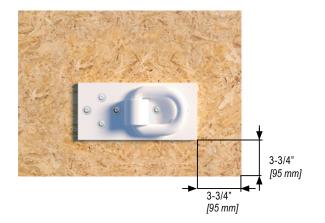
Lifting Device	Relative Density [G]	Minimum OSB Panel Thickness [ t <sub>oss</sub> ]			Fastener Opti	Basic Factored Resistance Value [ N', ]		
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
Mini Yoke ; 8 Screws	0.42 [SPF]							
	0.49 [D.Fir]	0.43"	[11]	SK	1/4" x 2"	[6 x 50]	141	[0.63]

#### Notes:

Step 2.A: Light Frame Panel Rigging

- 1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10
- 2. Listed basic factored resistance values ( $N'_r$ ) are only valid for limit state design in Canada
- 3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30
- 4. Listed basic factored resistance values (N',) are valid for sling angle to the panel ( $\beta$ ) of 60 °
- 5. Listed basic factored resistance values (N',) valid only with listed ASSY screws
- 6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift





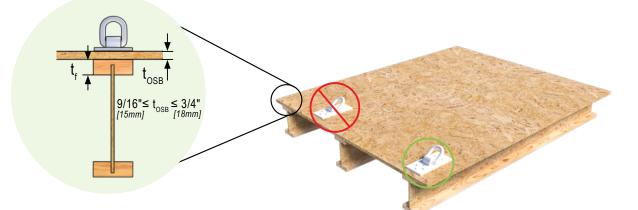
## Prefabricated I-Joist Floor Panels Using Yoke Systems

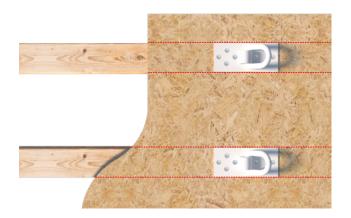
Table 5, Basic Factored Resistance Values for Prefab.I-Joist Floor Rigging Using Mini Yoke (N',)

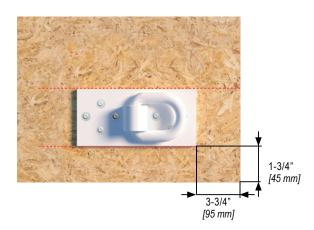
Lifting Device	Relative Density [G]	Minimum Flange Thickness			Fastener Option	Basic Factored Resistance Value [ N' <sub>r</sub> ]		
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
Mini Yoke ; 8 Screws	0.42 [SPF]							
N',	0.49 [D.Fir]	1.5"	[ 38 ]	SK	1/4" x 2-3/8"	[6×60]	715	[3.18]

#### Notes:

- 1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10
- 2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada
- 3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30
- 4. Listed basic factored resistance values (N',) are valid for sling angle to the panel ( $\beta$ ) of 60 °
- 5. Listed basic factored resistance values ( $N'_r$ ) valid only with listed ASSY screws
- 6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift
- 7. The Mini Yoke must only be placed so that screws properly penetrate both panel and I-joist flange, as the capacity of the Mini Yoke cannot be guaranteed in other configurations







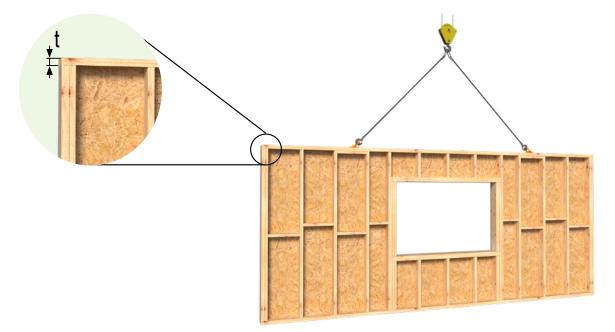
## Prefabricated Stud Walls Using Yoke Systems

Table 6, Basic Factored Resistance Values for Prefab.Stud Wall Rigging Using Yoke 1T (N',)

Lifting Device	Relative Density [G]	Minimum Penetration Thickness		Fastener Options		Resista	Factored nce Value N',]
		in	[ mm ]	in	[ mm ]	lbs	[ KN ]
Yoke 1T ; 2 Screws	0.42 [SPF]						
N'	0.49 [D.Fir]	3"	[76]	VG CSK 3/8" x 4"	[ 10 x 100 ]	1,245	[ 5.54 ]

#### Notes:

- 1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10
- 2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada
- 3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30
- 4. Listed basic factored resistance values ( $N'_r$ ) are valid for sling angle to the panel ( $\beta$ ) of 60 °
- 5. Listed basic factored resistance values (N',) valid only with listed ASSY screws
- 6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift
- 7. The minimum member thickness for proper fastener penetration as stated in Table 6 must be respected
- 8. All sheathing, blocking, sill, and top plates should be nailed or screwed appropriately for continuous load path
- 9. The capacity of this system is not guaranteed for panel tilt up





## Step 2, Option B: Mass Timber, Floor / Roof Panel Rigging CLT Panel Rigging Using Transport Anchor

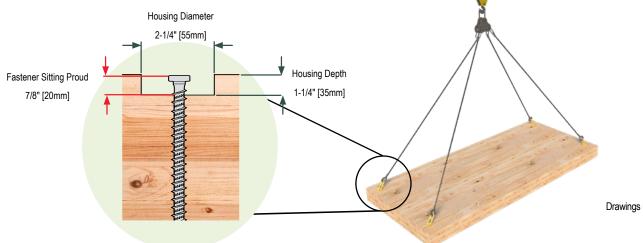
Table 7, Basic Factored Resistance Values for Flat CLT Panel Rigging Using Transport Anchor (TA) (N',)

Lifting Device	Relative Density [G]	Penet	mum tration tness	Fastener Options			Basic Factored Resistance Value [ N',]	
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
TA ; 1 Screw		3-1/8"	[78]	Kombi LT	1/2" x 3-1/8"	[12 x 80]	630	[ 2.8 ]
	0.42 [SPF]	4-3/4"	[ 120 ]	Kombi	1/2" x 4-3/4"	[12 x 120]	1,050	[ 4.6 ]
N',		6-1/4"	[ 160 ]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	1,350	[ 6.0 ]
90°	0.49 [D.Fir]	3-1/8"	[78]	Kombi LT	1/2" x 3-1/8"	[12 x 80]	630	[ 2.8 ]
		4-3/4"	[ 120 ]	Kombi	1/2" x 4-3/4"	[12 x 120]	1,050	[4.6]
		6-1/4"	[160]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	1,350	[6.0]
Housed TA ; 1 Screw	0.42	5-1/2"	[ 139 ]	Kombi	1/2" x 4-3/4"	[12 x 120]	1,050	[4.6]
N',	[SPF]	7-1/8"	[ 180 ]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	1,350	[6.0]
90°	0.49	5-1/2"	[ 139 ]	Kombi	1/2" x 4-3/4"	[12 x 120]	1,050	[4.6]
	[D.Fir]	7-1/8"	[ 180 ]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	1,350	[6.0]

#### Notes:

1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10

- 2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada
- 3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30
- 4. Listed basic factored resistance values (N',) are valid for sling angle to the panel ( $\beta$ ) of 60 °
- 5. Listed basic factored resistance values (N',) valid only with listed ASSY screws
- 6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift
- 7. Fastener head must sit proud 7/8" [20mm] from the surface of the panel for proper engagement of the anchor
- 8. Proper housing dimensions must be used as described on page 35
- 9. The Transport Anchor must be engaged and aligned with the axis angle of the lifting slings as described on page 35



Drawings Not to Scale

## **CLT Panel Rigging Using Yoke Systems**

Table 8, Basic Factored Resistance Values for Flat CLT Panel Rigging Using Yoke 1T (N',)

Lifting Device	Relative Density [G]	Minimum Penetration Thickness			Basic Fa Fastener Options Resistanc [ N'		ce Value	
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
Yoke 1T ; 2 Screws		3-1/8"	[78]	Kombi LT	1/2" x 3-1/8"	[12 x 80]	1,600	[71]
• <b>●</b>	0.42 [SPF]	4"	[100]	Kambi	1/2" x 4"	[12 x 100]	1,000	[7.1]
		4-3/4"	[120]	Kombi	1/2" x 4-3/4"	[12 x 120]	1,900	[8.5]
N', 🅖		6-1/4"	[160]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	2,200	[9.8]
		3-1/8"	[78]	Kombi LT	1/2" x 3-1/8"	[12 x 80]	2 400	1021
	0.49	4"	[100]	Kambi	1/2" x 4"	[12 x 100]	2,100	[9.3]
	[D.Fir]	4-3/4"	[120]	Kombi	1/2" x 4-3/4"	[ 12 x 120 ]	2,150	[9.6]
		6-1/4"	[160]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	2,200	[9.8]

#### Notes:

1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10

2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada

3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30

4. Listed basic factored resistance values (N',) are valid for sling angle to the panel ( $\beta$ ) of 60 °

5. Listed basic factored resistance values  $(N'_r)$  valid only with listed ASSY screws

6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift

#### Table 9, Basic Factored Resistance Values for Flat CLT Panel Rigging Using Yoke 5T (N',)

Lifting Device	Relative Density [G]	Minimum Panel Thickness			Fastener Option	ns	Basic Factored Resistance Value [ N',]	
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
Yoke 5T ; 4 Screws		3-1/8"	[78]	Kombi LT	1/2" x 3-1/8"	[12 x 80]	2 800	[125]
	0.42	4"	[100]	Kambi	1/2" x 4"	[12 x 100]	2,800	[12.5]
	[SPF]	4-3/4"	[120]	Kombi	1/2" x 4-3/4"	[12 x 120]	3,900	[17.3]
N'.		6-1/4"	[160]	Kombi LT	1/2" x 6-1/4"	[ 12 x 160 ]	7,000	[31.1]
		3-1/8"	[78]	Kombi LT	1/2" x 3-1/8"	[12 x 80]	3 100	[ 10 7 ]
	0.49	4"	[ 100 ]	Kambi	1/2" x 4"	[ 12 x 100 ]	3,100	[13.7]
	[D.Fir]	4-3/4"	[120]	Kombi	1/2" x 4-3/4"	[ 12 x 120 ]	4,300	[ 19.1 ]
	-	6-1/4"	[160]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	7,700	[ 34.2 ]

#### Notes:

1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10

2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada

3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30

4. Listed basic factored resistance values (N',) are valid for sling angle to the panel ( $\beta$ ) of 60 °

5. Listed basic factored resistance values (N',) valid only with listed ASSY screws

6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift

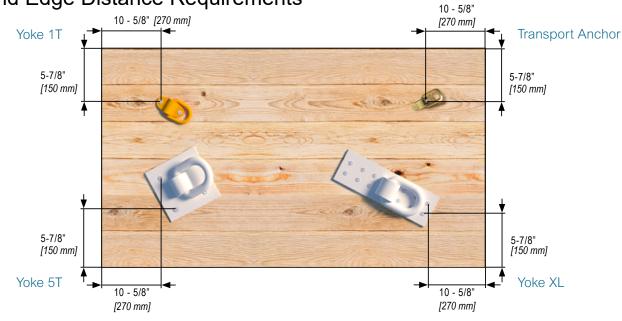
Lifting Device	Relative Density [G]	Pa	Minimum Panel Thickness		Fastener Option	าร	Basic Factored Resistance Value [ N' <sub>r</sub> ]		
		in	[ mm ]			in	[ mm ]	lbs	[ KN ]
Yoke XL ; 4 Screws		3-1/8"	[78]		Ecofast	3/8" x 3-1/8"	[10 x 80]	1,800	[ 8.0 ]
	0.42 [SPF]	4"	[ 100 ]		VG CSK	3/8" x 4"	[10 x 100 ]	3,500	[ 15.6 ]
N' A		6-1/4"	[ 160 ]		VG CSK -	3/8" x 6-1/4"	[10 x 160]	6,300	[ 28.0 ]
		3-1/8"	[ 78 ]		Ecofast	3/8" x 3-1/8"	[ 10 x 80 ]	1,900	[ 8.4 ]
	0.49 [D.Fir]	4"	[ 100 ]		VG CSK	3/8" x 4"	[ 10 x 100 ]	4,000	[17.8]
		6-1/4"	[ 160 ]			3/8" x 6-1/4"	[ 10 x 160 ]	7,000	[ 31.1 ]
Yoke XL ; 8 Screws		3-1/8"	[ 78 ]		Ecofast	3/8" x 3-1/8"	[ 10 x 80 ]	3,700	[16.4]
	0.42 [SPF]	4"	[ 100 ]			3/8" x 4"	[ 10 x 100 ]	6,700	[ 29.8 ]
N'. A		6-1/4"	[160]		VG CSK	3/8" x 6-1/4"	[ 10 x 160 ]	10,100	[ 44.9 ]
		3-1/8"	[78]		Ecofast	3/8" x 3-1/8"	[ 10 x 80 ]	4,100	[18.2]
	0.49 [D.Fir]	4"	[ 100 ]			3/8" x 4"	[ 10 x 100 ]	7,600	[ 33.8 ]
		6-1/4"	[ 160 ]		VG CSK	3/8" x 6-1/4"	[ 10 x 160 ]	10,500	[46.7]
Yoke XL ; 12 Screws		3-1/8"	[78]		Ecofast	3/8" x 3-1/8"	[ 10 x 80 ]	5,500	[ 24.4 ]
•••	0.42 [SPF]	4"	[ 100 ]		NO 0014	3/8" x 4"	[10 x 100 ]	10,400	[ 46.3 ]
N'. <i>R</i>		6-1/4"	[ 160 ]		VG CSK	3/8" x 6-1/4"	[10 x 160]	10,900	[ 48.5 ]
	0.49 [D.Fir]	3-1/8"	[78]		Ecofast	3/8" x 3-1/8"	[ 10 x 80 ]	5,800	[ 25.8 ]
		4"	[ 100 ]			3/8" x 4"	[10 x 100 ]	10,600	[ 47.2 ]
		6-1/4"	[ 160 ]		VG CSK -	3/8" x 6-1/4"	[10 x 160]	11,000	[ 48.9 ]

#### Table 10, Basic Factored Resistance Values for Flat CLT Panel Rigging Using Yoke XL (N',)

Notes:

1. See notes under table 9

2. For the different screw options of the Yoke XL system, the screws must be placed in the holes as specified in table 10



## MPP Panel Rigging Using Yoke Systems

Table 11, Basic Factored Resistance Values for Flat MPP Panel Rigging Using Yoke XL (N',)

Lifting Device	Relative Density [G]		Minimum Panel Fhickness	Fastener Options			Basic Factored Resistance Value [ N',]	
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
Yoke XL ; 8 Screws		2"	[51]	SK	5/16" x 2-3/8"	[8 x 60]	1,820	[8.1]
N',	0.42 [SPF]	4"	[100]		3/8" x 4"	[10 x 120]	4,620	[20.6]
		6"	[ 152 ]	VG CSK	3/8" x 6-1/4"	[10 x 160]	7,000	[31.2]
Yoke XL ; 12 Screws		2"	[51]	SK	5/16" x 2-3/8"	[8 x 60]	2,800	[12.5]
N',	0.42 [SPF]	4"	[100]		3/8" x 4"	[10 x 120]	7,000	[31.1]
		6"	[ 152 ]	VG CSK	3/8" x 6-1/4"	[10 x 160]	9,800	[ 42.6]

#### Notes:

1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10

2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada

3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30

4. Listed basic factored resistance values (N'\_r) are valid for sling angle to the panel ( $\beta$ ) of 60 °

5. Listed basic factored resistance values (N',) valid only with listed ASSY screws

6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift

7. For the different screw options of the Yoke XL system, the screws must be placed in the indicated holes in table 11



## CLT Wall Panel Tilting From Edge Using Yoke Systems

Table 12, Basic Factored Resistance Values for CLT Wall Panel Tilting Using Yoke XL on Panel Edge (N',)

Lifting Device	Relative Density [G]	Pa	mum Inel kness	Fastener Options		15	Basic Factored Resistance Value [ N',]	
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
Yoke XL ; 12 Screws	0.42 [SPF]	3-1/2"	[ 87 ]	VG CSK	3/8" x 6-1/4"	[10 x 160]	2,800	[ 12.4 ]
Notes:	0.49 [D.Fir]	3-1/2"	[87]	VG CSK	3/8" x 6-1/4"	[10 x 160]	3,100	[13.8]

1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10

2. Listed basic factored resistance values ( $N'_{r}$ ) are only valid for limit state design in Canada

3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30

4. Listed basic factored resistance values (N',) are valid for sling angle to the panel ( $\beta$ ) of 60 °

5. Listed basic factored resistance values (N',) valid only with listed ASSY screws

6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift

7. Listed basic factored resistance values (N',) assume the panel is tilted while one end is bearing on a stable surface





## End And Edge Distance Requirements

For wall panel rigging on the narrow edge of CLT panels, only the Yoke XL is used since it uses small diameter fasteners. The reduced edge distance requirements below are a minimum and apply to the Yoke XL only.



## CLT Wall Panel Tilting From Face Using Yoke Systems

Table 13, Basic Factored Resistance Values for Lifting CLT Wall Panels with Yoke XL on Panel Face (N',)

Lifting Device	Relative Density [G]	Minimum Panel Thickness		Fastener Options			Basic Factored Resistance Value [ N',]	
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
Yoke XL ; 12 Screws	0.42	4"	[ 100 ]		3/8" x 4"	[10 x 100]	0.570	145.01
	[SPF]	6-1/4"	[ 160 ]	VG CSK	3/8" x 6-1/4"	[10 x 160]	3,570	[ 15.9 ]
N',	0.49 [D.Fir]	4"	[ 100 ]	VC CSK	3/8" x 4"	[10 x 100]	2 955	[ 47 4 ]
		6-1/4"	[ 160 ]	VG CSK	3/8" x 6-1/4"	[10 x 160]	3,855	[17.1]

#### Notes:

1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10

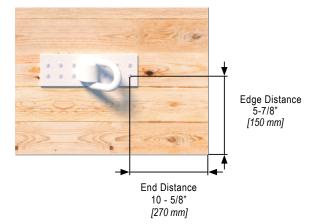
- 2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada
- 3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30
- 4. Listed basic factored resistance values (N'<sub>r</sub>) are valid for sling angle to the panel ( $\beta$ ) of 60 °
- 5. Listed basic factored resistance values (N',) valid only with listed ASSY screws
- 6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift
- 7. Listed basic factored resistance values (N',) assume the panel is tilted with the anchors placed on the panel face while one end is bearing on a stable surface
- 8. Screw length and panel thickness must be considered to prevent through penetration of the screw

#### Tilting up CLT wall panels from side with the Yoke XL









## MPP Wall Panel Tilting From Side Using Yoke Systems

Table 14, Basic Factored Resistance Values for Lifting MPP Wall Panels with Yoke XL on Panel Face (N',)

Lifting Device	Relative Density [G]	P	imum anel :kness	Fastener Options			Basic Factored Resistance Value [ N',]		
		in	[ mm ]			in	[ mm ]	lbs	[ KN ]
Yoke XL ; 12 Screws		2"	[51]		SK	5/16" x 2-3/8"	[8 x 60]	3,220	[ 14.3 ]
N',	0.42 [SPF]	4"	[100]			3/8" x 4"	[ 10x 100 ]	4,300	[ 19.1 ]
		6"	[ 152 ]		VG CSK	3/8" x 6-1/ 4"	[ 10 x 160 ]	4,300	[ 19.1 ]

#### Notes:

1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10

2. Listed basic factored resistance values  $(N'_r)$  are only valid for limit state design in Canada

3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30

4. Listed basic factored resistance values (N',) are valid for sling angle to the panel ( $\beta$ ) of 60 °

5. Listed basic factored resistance values (N',) valid only with listed ASSY screws

6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift

7. Listed basic factored resistance values (N',) assume the panel is tilted with the anchors placed on the panel face while one end is bearing on a stable surface

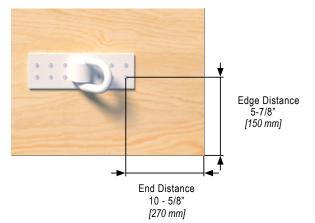
8. Screw length and panel thickness must be considered to prevent through penetration of the screw

#### Tilting up MPP wall panels from side with the Yoke XL









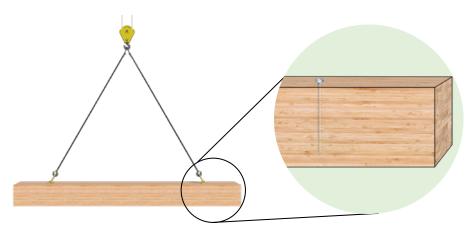
## Step 2, Option D: Glulam Beam & Log Rigging

# Table 15, Basic Factored Resistance Values for Glulam Beam & Log Rigging Using Transport Anchor (TA) Screws at 90 Degrees (N',)

Lifting Device	Relative Density [G]	Minimum Element Thickness			Fastener Options			actored ce Value ',]
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
TA ; 1 Screw				Kombi LT	1/2" x 3-1/8"	[ 12 x 80]	630	[ 2.8 ]
	0.42 [SPF]	6-5/8"	[168]	Kombi	1/2" x 4-3/4"	[12 x 120]	1,050	[4.7]
ØN',				Kombi LT	1/2" x 6-1/4"	[12 x 160]	1,400	[6.2]
				Kombi LT	1/2" x 3-1/8"	[ 12 x 80]	630	[ 2.8 ]
90°	0.49 [D.Fir]	6-5/8"	[ 168 ]	Kombi	1/2" x 4-3/4"	[12 x 120]	1,050	[4.7]
				Kombi LT	1/2" x 6-1/4"	[12 x 160]	1,400	[6.2]

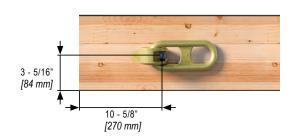
#### Notes:

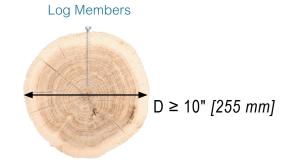
- 1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10
- 2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada
- 3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30
- 4. Listed basic factored resistance values (N'<sub>r</sub>) are valid for sling angle to the panel ( $\beta$ ) of 60 °
- 5. Listed basic factored resistance values (N',) valid only with listed ASSY screws
- 6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift
- 7. Listed basic factored resistance values (N',) are valid for screws installed at 90° to the beam or log surface
- 8. Fastener head must sit proud 7/8" [20mm] from the surface of the rigging element for proper engagement of the anchor
- 9. The Transport Anchor must be engaged and aligned with the axis angle of the lifting slings as described on page 35
- 10. Listed basic factored resistance values (N',) are valid for logs with a minimum 10" diameter



### End and Edge Distance Requirements

#### Glulam Members



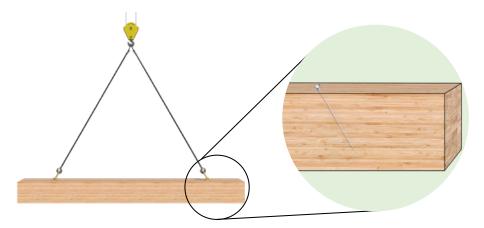


#### Table 16, Basic Factored Resistance Values for Glulam Beam & Log Rigging Using Transport Anchor (TA) Screw at 60 Degrees (N'.)

Lifting Device	Relative Density [G]	Minimum Element Thickness			Fastener Optio	ns	Basic Factored Resistance Value [ N',]			
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]		
TA ; 1 Screw	0.42		[ 168 ]			Kombi	1/2" x 4-3/4"	[12 x 120]	1,150	[5.1]
CDD الم	0.42 [SPF]	6-5/8"		Kombi LT	1/2" x 6-1/4"	[12 x 160]	1,620	[7.2]		
60°	0.49	6-5/8"		[ 169 ]	Kombi	1/2" x 4-3/4"	[12 x 120]	1,150	[5.1]	
	[D.Fir]	0-5/0	[ 168 ]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	1,620	[7.2]		

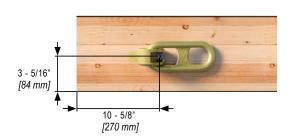
Notes:

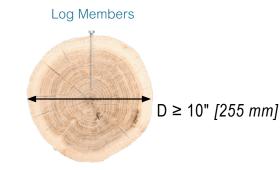
- 1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10
- 2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada
- 3. Listed basic factored resistance values (N',) must be factored with appropriate reduction factors as described on page 30
- 4. Listed basic factored resistance values (N'\_r) are valid for sling angle to the panel ( $\beta$ ) of 60 °
- 5. Listed basic factored resistance values (N',) valid only with listed ASSY screws
- 6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift
- 7. Listed basic factored resistance values (N',) are valid for screws installed at 60° to the beam or log surface
- 8. Fastener head must sit proud 7/8" [20mm] from the surface of the rigging element for proper engagement of the anchor
- 9. The Transport Anchor must be engaged and aligned with the axis angle of the lifting slings as described on page 32
- 10. Listed basic factored resistance values (N',) are valid for logs with a minimum 10" diameter



### End and Edge Distance Requirements

#### Glulam Members







Lifting Device	Relative Density [G]	Minimum Beam Width <b>in [</b> mm ]			Fastener Options		Basic Factored Resistance Value [ N' <sub>r</sub> ]	
					in	[ mm ]	lbs	[ KN ]
Yoke 1T ; 2 Screws	0.42			Kombi	1/2" x 4-3/4"	[12 x 120]	1,900	[ 8.5 ]
<b>●●</b>	[SPF]	6-5/8"	[ 168 ]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	2,200	[ 9.8 ]
	0.49	6-5/8"		Kombi	1/2" x 4-3/4"	[12 x 120]	2,150	[9.6]
	[D.Fir]	0-0/0	[168]	Kombi LT	1/2" x 6-1/4"	[12 x 160]	2,200	[ 9.8 ]

Notes: 1. See notes under table 18

Table 18, Basic Factored Resistance Values for Glulam Beam Rigging Using Yoke XL (N',)

	Relative Density [G]	Ве	mum am dth		Fastener Option	ns	Basic Factored Resistance Value [ N' <sub>r</sub> ]	
		in	[ mm ]		in	[ mm ]	lbs	[ KN ]
Yoke XL ; 4 Screws	0.42	F 4/07	[ 130 ]		3/8" x 4"	[10 x 100 ]	3,500	[ 15.8 ]
N', A	[SPF]	5-1/8"	[130]	VG CSK -	3/8" x 6-1/4"	[10 x 160]	6,300	[ 28.0 ]
	0.49	E 4/0"	[ 130 ]		<b>3/8" x 4</b> " [10 x 100 ] <b>4,000</b>	[17.8]		
	[D.Fir]	5-1/8"	[ 100 ]	VG CSK	3/8" x 6-1/4"	[10 x 160]	7,000	[31.1]
Yoke XL ; 12 Screws	0.42	F 4/0"	[ 420 ]		3/8" x 4"	[10 x 100]	10,400	[ 46.3 ]
N', <i>M</i>	[SPF]	5-1/8"	[ 130 ]	VG CSK -	3/8" x 6-1/4"	[10 x 160]	10,900	[ 48.5 ]
	0.49	E 4/0"	[ 120 ]		3/8" x 4"	[10 x 100]	10,600	[ 47.2 ]
	[D.Fir]	5-1/8"	[130]	VG CSK	3/8" x 6-1/4"	[10 x 160]	10,600 [ 47.2	[ 48.9 ]

Notes:

1. All rigging design must meet relevant requirements of the General Notes to Designer section, page 10

2. Listed basic factored resistance values (N',) are only valid for limit state design in Canada

3. Listed basic factored resistance values (N') must be factored with appropriate reduction factors as described on page 30

4. Listed basic factored resistance values (N',) are valid for sling angle to the panel ( $\beta$ ) of 60 °

5. Listed basic factored resistance values (N',) valid only with listed ASSY screws

6. The resistance of ASSY screws is only assured for a single use. New screws must be used for each lift

7. For the different screw options of the Yoke XL system, the screws must be placed in the holes as specified in table 18



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## Step 3: Safety Checks

#### Step 3, Check A: Screw Penetration

Fastener length is often limited by the thickness of the rigged element. While it is recommended that the screws should penetrate as many plies as possible, a minimum clearance of 10mm is recommended to avoid through penetration of the screw. The following tables provide suggested fastener lengths for most common North American MPP and CLT thicknesses.

Table 19, ASSY Screw Length Suggestion According to MPP Panel Thickness With Yoke XL Anchor

MPP Pane	I Туре	Rigging Device				
Thickne	ess		Yoke XL			
in	[ mm ]	Fastener	in	[ mm ]		
2"	[51]	SK	5/16" x 2-3/8"	[8 x 60]		
4"	[100]	VG CSK ·	3/8" x 4"	[ 10 x 100 ]		
6"	[ 152 ]	VG CSK	3/8" x 6-1/4"	[ 10 x 160 ]		

Notes:

1. Fastener lengths are suggestions only and can be adapted to fit certain site conditions and rigging needs

2. The thread embedment length on the fastener determines the capacity of each system

#### Table 20, ASSY Screw Length Suggestion According to CLT Panel Thickness With Transport Anchor

С	LT Pane	Туре	Rigging Device						
Thickness		iness	Transport An	Transport Anchor Transport Anchor - With Hous					
	in	[ mm ]	Fastener in	[ mm ]	Fastener	in	[ mm ]		
	3-1/8"	[78]							
	3-3/8"	[87]							
L L	3-1/2"	[ 89 ]	Kombi LT 1/2" x 3-1/8'	' [12 x80 ]		N/A			
о С С	4"	[ 100 ]				N/A			
	4-1/8"	[ 105 ]							
	4-3/4"	[120]	Kombi 1/2" x 4-3/4	[ 12 x120 ]					

	4"	[ 100 ]		Kombi LT	1/2" x 3-1/8"	[ 12 x80 ]			N/A	
	4-3/4"	[120]		Kombi			Kombi <b>1/2" x 4</b> "	1/2" x 4"	[ 12 x100 ]	
	5-1/8"	[131]			1/2" x 4-3/4"	[10 110]			1/2" x 4-3/4"	[12 x120]
	5-1/2"	[ 139 ]		NUTIDI	1/2 X 4-3/4	[12 x120]		Kombi		
5 P	5-5/8"	[143]								
	6-1/4"	[160]								
	6-7/8"	[175]		Kombi LT	1/2" x 6-1/4"	[ 12 x160 ]		Kombi I T	T 1/2" x 6-1/4"	[12 x160]
	7-1/8"	[ 180 ]								

Notes

1. Fastener lengths are suggestions only and can be adapted to fit certain site conditions and rigging needs

2. The thread embedment length on the fastener determines the capacity of each system

#### Table 21, ASSY Screw Length Suggestion According to CLT Panel Thickness With Yoke Anchors

C	LT Panel	Panel Type Rigging Devic						Rigging Device	)					
Thickness		Yoke 1T				Yoke 5T			Yoke XL					
	in	[ mm ]	F	astener	in	[ mm ]	1	Fastener	in	[ mm ]	1	astener	in	[ mm ]
	3-1/8"	[78]									-	Ecofast	3/8" x 3-1/8"	[ 10 x 80 ]
	3-3/8"	[87]		Kombi LT	1/2" x 3-1/8"	[ 12 x80 ]		Kombi LT	1/2" x 3-1/8"	[ 12 x80 ]		Ecolasi	3/0 X 3-1/0	[10 x 80]
	3-1/2"	[ 89 ]												
ц В С	4"	[ 100 ]		Kombi	1/2" x 4"	[ 12 x100 ]		Kombi	1/2" x 4"	[ 12 x100 ]		VG CSK	3/8" x 4"	[ 10 100 ]
	4-1/8"	[ 105 ]		NUTIDI	1/2 14	[12 x100]		NUTIDI	1/2 84	[12 x100]		VGCSK	J/U X 4	[10 x 100]
	4-3/4"	[120]		Kombi	1/2" x 4-3/4"	[ 12 x120 ]		Kombi	1/2" x 4-3/4"	[12 x120]				

	4"	[100]	ł	Kombi	1/2" x 4"	[12 x100]	Kombi	1/2" x 4"	[12 x100 ]			
	4-3/4"	[120]										
	5-1/8"	[131]	L.	Kombi	1/2" x 4-3/4"	[ 12 × 120 ]	20] Kombi <b>1/2" x 4-3/4</b> " [12 x 3	[ 12 v120 ]	VG CSK	3/8" x 4"	[10 x 100]	
≻.	5-1/2"	[ 139 ]	r	NOTIDI	1/2 X 4-3/4	[12 x120]	KUTIDI	1/2 X 4-3/4	[12 x120]			
Б	5-5/8"	[143]										
2	6-1/4"	[160]										
	6-7/8"	[175]	Ka	ombi I T	1/0" v 6 1/4"	[ 12 × 160 ]	KombilT	1/2" x 6-1/4"	[ 12 ×160 ]	VC CSK	2/0" x 6 4/4"	[10 x 160]
	7-1/8"	[180]	ĸ		1/2" x 6-1/4"	[12 x100]	Kombi LT	1/2 x 0-1/4	[12 x160]	VGCSK	3/8" x 6-1/4"	[10 x 100]
	7-7/8"	[ 200 ]										

	4-3/8"	[ 111 ]	Kombi	1/2" x 4"	[12 x100]	Kombi	1/2" x 4"	[12 x100 ]	VG CSK	3/8" x 4"	[10 x 100]
	7-1/2"	[191]									
Ľ	7-3/4"	[197]									
7 P	8-3/8"	[213]	Kombi LT	1/2" x 6-1/4"	[12 x160]	Kombi LT	1/2" x 6-1/4"	[12 x160]	VG CSK	3/8" x 6-1/4"	[10 x 160]
	8-5/8"	[220]									
	9-5/8"	[245]									

Notes:

1. Fastener lengths are suggestions only and can be adapted to fit certain site conditions and rigging needs

2. The thread embedment length on the fastener determines the capacity of each system

Kombi LT 1/2" x 6-1/4"	emmunumunum	VG CSK 3/8" x 6-1/4"
Kombi 1/2" x 4-3/4"		VG CSK 3/8" x 4"
Kombi 1/2" x 4"		Ecofast 3/8" x 3-1/8"
Kombi LT 1/2" x 3-1/8"		SK 5/16" x 2-3/8"

SK 1/4" x 2-3/8"

### Step 3, Check B: System Capacity

$$N_{r} = N'_{r} \cdot n \cdot R_{AR} \cdot R_{LS} \cdot R_{D}$$
 (eq.3)

- Anchor(s) capacity Nŗ
- **N'**, Basic factored resistance per anchor (provided in design tables)
- n Number of anchors used
  - Anchor resistance reduction factor:
    - For sling angles ≥60° to the panel surface

1.0

1.0

0.86

• For one [or more] sling angles <60° to the panel surface

β	50°	40°	30°	20°	10°	20°
R <sub>AR</sub>	0.8	0.65	0.55	0.45	0.35	0.3
Notes:						

Not applicable for the Transport Anchor 1.

 $\mathbf{R}_{\mathrm{LS}}$ Load spreader reduction factor:

• For n = 2	1.0
<ul> <li>For n = 4, with adequate load spreader/compensation device</li> </ul>	1.0
<ul> <li>For n = 4, without adequate load spreader/conpensation device</li> </ul>	0.5

#### Load duration reduction factor: $\mathbf{R}_{D}$

- Short term rigging (<10 min)
- Long term rigging (>10 min)

 $\mathbf{R}_{_{\mathrm{AR}}}$ 

## Step 3, Check C: Sling Angle Loading (S)

The values listed for the rigging devices account for the forces applied on the anchors themselves and are valid for rigging scenarios with a minimum sling angle ( $\beta$ ) of 60°, where ( $\beta$ ) is measured between the sling and the panel surface. The working limits of common sling configurations can be estimated using simple geometry of the rigged element. The simplified modification factor based on the sling angle loading (S) is shown in Table 23.

Sling Angle (β)	Modification Factor Per Leg of Sling
90°	1.00
75°	1.03
60°	1.15
45°	1.43
30°	2.00

Table 23, Modification Factor for Sling Angles Loading (S)

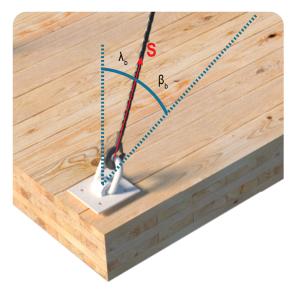
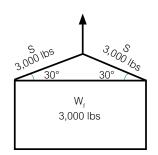


Table 24 demonstrates sling angle working limits when lifting an assumed 3,000lbs wall panel on the narrow edge using two anchors. The load per one leg of sling for an angle of 60° is calculated using half of the panel weight divided by the sine of 60°. It is clear from Table 24 that slings with an angle to the surface of less than 60° have smaller sling working limits and exceed the total element weight. Therefore, usage of sling angles less than 60° must be avoided and is not recommended for safe rigging applications.

Table 24,	Example	Sling Angle	Loading
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Sling Angle (β)	Assumed Factored Total Load [W <sub>f</sub> ]	Load Per Leg of Sling [S]
	lbs	lbs
90°		1,500
75°		1,553
60°	3,000	1,732
45°		2,124
30°		3,000



Example Sling Angle Simplified

It is crucial for the designer to ensure the anchor capacity (N<sub>r</sub>) found in Step 3, Check B exceeds the total summation of all sling forces ( $S_T$ ):

$$S_{T} = \Sigma S$$
  
 $N_{r} > S_{T}$ 

### Step 3, Check D: On-site Safety Inspection

### General

All rigging devices must be examined frequently by a trained safety professional. Additional inspection of devices prior to each lift is suggested to ensure a safe lifting procedure and proper quality control. Anchors must be inspected for any damages (external wear, cuts, cracks, etc.). If the anchor is deemed to be damaged, the device must be taken out of circulation immediately.

Anchors must be safely transferred between lifts to prevent damages or micro cracks that can compromise the overall anchor capacity and cause potential safety hazards. If proper inspection is done, anchors can be re-used on multiple rigging projects. However, the fasteners used for panel rigging must only be used once to ensure safety and proper system capacity.

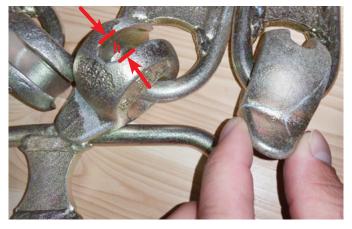
#### Yoke System

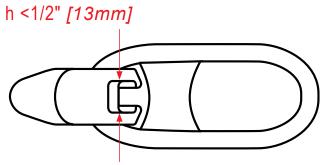
Yoke anchors must be inspected for any damages to the powder-coated finish and for any corrosion that may affect system capacity. Repair or modification of any kind to the Yoke systems, particularly welding, is not permitted.

### Transport Anchor System

The Transport Anchor must be inspected for any damages to the galvanized finish and for any corrosion that may affect system capacity. Repair or modification of any kind to the Transport Anchor, particularly welding, is not permitted.

The Transport Anchor receiver mouth width "h" must not exceed 1/2" (13mm). If inspection concludes that the width of the receiver mouth is greater than 1/2" (13mm), the Transport Anchor must be taken out of circulation immediately. A larger receiver mouth cannot properly engage the screw during rigging and can cause potential safety hazards. The following image of damaged Transport Anchors highlights this concept.





# Meadows Community Recreation Centre

Edmonton, Alberta

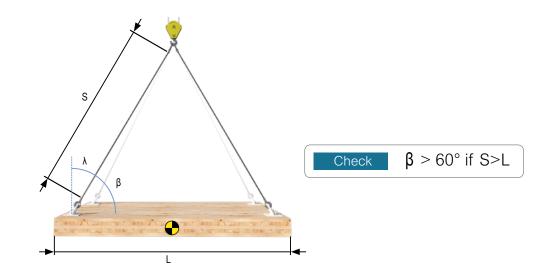
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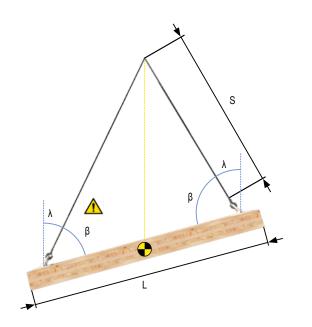
# **Step 4: Installation Instructions**

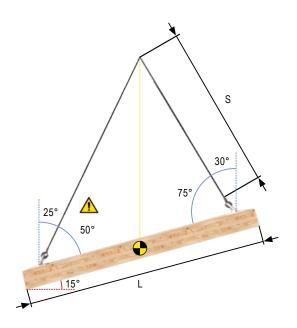
### Step 4, Check A: Sling Angle Installation

Tabulated basic factored resistance (N'<sub>r</sub>) values are valid for rigging scenarios with a minimum sling angle ( $\beta$ ) measured between the sling and the panel surface of 60°. If length S is greater than L as illustrated in the figure below,  $\beta$  angles bigger than 60° will be achieved.



For cases where the sling angle ( $\beta$ ) is less than 60°, an appropriate reduction factor ( $R_{AR}$ ) must be applied to the capacity of the anchors ( $N_r$ ).





Example of Panel Angled at 15°

# Step 4, Check B: Load Spreading

When using more than two anchors, it is important to avoid uneven load sharing. Without an adequate load spreader/compensation system, load may be unevenly distributed forcing the entire load into two slings while the remainder hang slack. In such cases, a reduction factor  $R_{LS} = 0.5$  will need to be applied to the basic factored resistance (N'<sub>r</sub>) of the anchors.



Example of uneven load sharing

### For Floor Panels

When lifting CLT floor panels using load spreader or compensation devices as seen below, even load share may be assumed.

### For Wall Panels

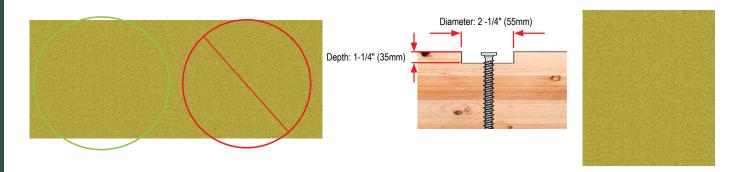
When lifting CLT wall panels, load spreaders can be used to further stabilize the load while increasing the sling angle ( $\beta$ ).





# Step 4, Check C: Transport Anchor Housing

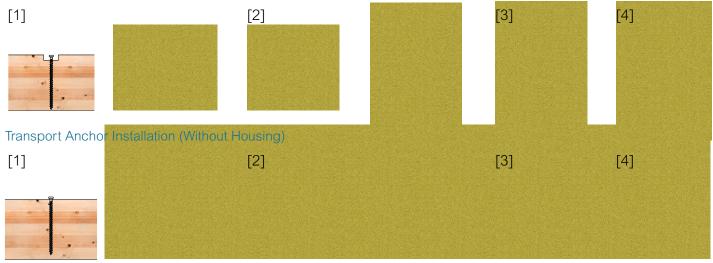
The Transport Anchor can be placed on the surface of the rigged element for a simple and easy installation. It can also be installed in a pre-cut circular housing for a flush finish. This allows the screw to be left installed but out of the way after lifting the element into place. A circular housing dimension of 1-1/4"" [30mm] deep and 2-1/4" [55mm] in diameter is suggested. In both cases (with housing or without housing) the anchor must always be engaged properly during lifting and any misalignment with the axis angle of the lifting slings must be avoided, as shown in the figure below. Additionally, the fastener head must sit proud 7/8" [20mm] from the surface of the panel for proper engagement of the anchor.



Installation of the Transport Anchor typically involves four general steps as shown below:

- [1] The screw is installed 7/8" [20mm] proud of the panel surface and the anchor is engaged
- [2] The anchor loop is aligned with the proper sling angle (perpendicular or inclined loading)
- [3] After lifting, the Transport Anchor is unhooked from the screw for removal
- [4] lifting screw is removed (optional)





### Transport Anchor Installation With Inclined Screw (Without Housing)



# Philip J. Currie Dinosaur Museum

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Wembley, Alberta

SNI/

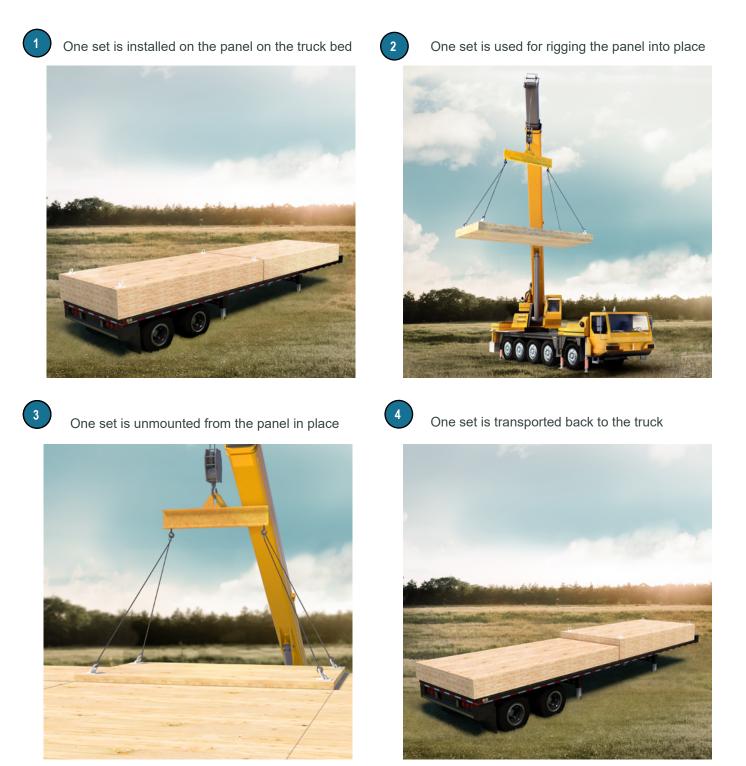
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# **Detailing Section**

### **On-site Considerations**

# **Recommended Workflow**

The prefabrication of various mass timber elements allows for a fast and efficient installation on-site. Most mass timber manufacturers consider sequencing of material, with the trucks arriving in the sequence in which the elements are set to be installed. During rigging, it is advantageous to keep up with the material workflow by steadily unloading truck beds and maximizing crane efficiency. Considering this, it is recommended to follow a circular workflow using four sets of rigging hardware to reduce delays on-site.



# Accessories

### **Magnetic Socket**

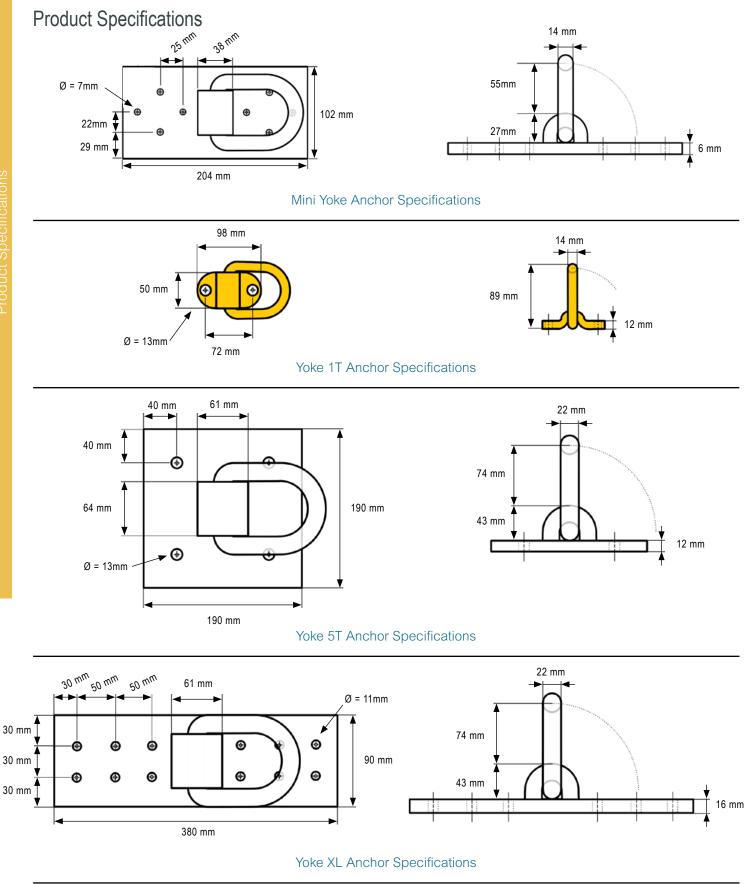
The Magnetic Socket can be used for faster installation of the ASSY Kombi screws used with the Yoke 1T, Yoke 5T and the Transport Anchor rigging devices. The built-in magnet allows the screw head to be placed snug inside the socket for a more optimized installation of the self-tapping screw.



# **Pre-fabricated Jigs**

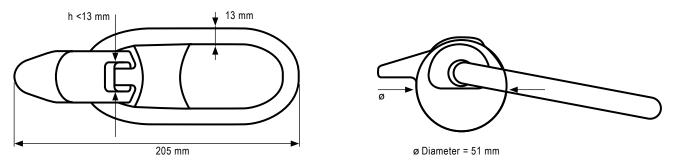
A jig can be prefabricated for repetitive lifts using the Yoke rigging systems as shown in the figure below. The jig can assist with the correct placement of the device on the element and ensure proper load sharing between all rigging devices. Additionally, faster workflow and installation may be accomplished on bigger projects with the use of a prefabricated jig.





Notes:

1. Drawings are not to scale

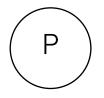




Product Specification

## Checklist

#### Factoring Total Loads



- Identify unfactored element weight
- □ Is the weight factored up with correct modification factors?
- □ Apply dynamic acceleration factors
- Apply optional safety factors

#### Anchor Selection



- □ Is the capacity per anchor enough to lift the element?
- □ Is the correct fastener length and type used?
- □ Is the minimum element thickness for lifting respected?
- Are geometry requirements satisfied?

### Safety Checks



- □ Is the correct number of anchors used?
- $\square$  Is the angle ( $\beta$ ) measured between the sling and the panel surface greater than 60°?
- $\square$  Is the angle ( $\lambda$ ) measured between the vertical and the sling smaller than 30°?
- □ Is the load rating of the slings greater than the angled force component?
- Is even load sharing between the anchors assured?
- □ Is the center of gravity below the upper pick point of the crane?

### **Rigging Hazards**



- □ Are the fasteners new? Fasteners must only be used once!
- □ Are all rigging devices inspected for damages prior to each lift?
- □ Is all rigging hardware installed properly and double checked?
- □ Is the surrounding area clear and safe?
- **D** Is the rigging element secured with tag lines?
- Does the current wind condition allow for safe rigging?
- **D** Is the intended location prepared to accept the rigged material?
- □ Is the panel fully secured with no load on the rigging slings?
- □ Are the used fasteners disposed of correctly to avoid reuse in future rigging applications? (Fasteners must only be used once!)

Kwantlen Polytechnic University

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Richmond, British Columbia

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